# HP MODEL 8690A SWEEP OSCILLATORS <br> Serials Below 803-2061 <br> Improved +275 V/-300 V Power Supplies 

A new improved Low Voltage Power Supply Assembly, HP Part Number 08690-6043, is the recommended replacement for Low Voltage Power Supply Assemblies A5 and A6, HP Part Numbers 08690-6015 and 08690-6024. The new assembly has improved reliability and stability, and is directly interchangeable with the old power supply.

The entire new assembly, consisting of Boards A5 and A6, must be installed at the same time. Neither of the new assemblies will work with one of the old A5 or A6 Assemblies.

The following pages contain complete theory of operation, troubleshooting flow diagram, replaceable parts list, and schematics for the new power supply.

AFTER INSTALLING THE NEW POWER SUPPLY, ATTACH THIS SERVICE NOTE TO YOUR 8690A SWEEP OSCILLATOR OPERATING AND SERVICE MANUAL.

MS/mh/wo 4/68-4

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| From: Tom Clyde, South Queensferry. | dare | 17th June, 1968, |
| :--- | ---: | :--- |
| To: All Service Facilities | subject: | 8690A Signal Generator |

Service Note P-08690-6043 issued by Microwave Division, also applies to 8690A's manufactured at South Queensferry. Our Serial Prefixes are different, however:-

> Service Note
> $P-08690 A-6043$

South Queensferry Prefix

U803-00401 and below

Regards, 70 m

## GENERAL POWER SUPPLY OPERATING PRINCIPLES

All the dc operating voltages shown in Figure 4-2 of the 8690A Operating and Service Manual are electronically regulated. Some are obtained directly from regulated supplies, others are derived by voltage division from regulated supplies.

There are five transistor type regulators, two vacuum tube types supplying +275 volts and -300 volts, and three transistor types supplying $+20,12.6$ and -6.3 volts. All of the regulators operate as follows. As shown in Figure 4-14 of the Operating and Service Manual, aregulating element (Series Regulator) is connected in series with the load and the dc power source (Rectifier). The resistance of the regulating element is made adjustable so that the voltage at its output will be adjustable. The resistance is adjusted by a control voltage; the higher the control voltage, the higher the output voltage. A sample of the Series Regulator output voltage is compared against a stable dc reference voltage by a Comparison Amplifier and the difference voltage is inverted and applied to the Series Regulator。As a result, any tendency for output voltage to change is immediately counteracted by the control voltage, and the supply output voltage remains constant.

Since the gain of the Comparison Amplifier determines the degree of regulation, it may be followed by an additional control, or driver, amplifier to improve regulation. The Comparison Amplifier is a differential type for temperature stability. The dc reference voltage used for comparison is obtained from voltage regulator electron tubes, from semiconductor voltage reference diodes, or by voltage division from another regulated power supply. When an adjustable power supply is used as the reference for another supply, changing its output level also changes the level of the supply for which it is the reference.
+275 AND -300V POWER SUPPLY TURN-ON SEQUENCE.

The following paragraphs describe the +275 V power supply. A similar description applies to the -300V supply, with exceptions noted.

A5CR1, A5CR2 and A5CR3 form a voltage reference stick, and provide +180 V to forward bias A5CR20. Current flows through A5R29 and A5R24, and then into the base of A6Q7. A5V1 will not conduct at first because filaments have not heated.
, The resulting large A6Q7 base current (about 0.9 mA ) causes A6Q7 to saturate. The high A8Q7 collector current robs base current from A6Q6 and shuts off series regulator A6Q10 by making A6Q5 and A6Q10 collector currents zero. This prevents current flow through the series regulator. Because A6Q10 is cut off, the impedance of the power supply is high and very little current flows through A5R34 into the +275V supply load.

Voltage at A6F1 (input to the +275 V supply voltage limiter) is about 360 V . Thus, current flows through A5R2, A6CR4, A6CR5, A6R6 and A6Q7. Initial +40V output voltage is established by voltage division between A5R2 and A6R6. The output voltage stays at about 40 V magnitude (+ for +275 V supply; - for -300 V supply) until after A5V1 vacuum tube filaments have heated up. The output voltages track as they increase from the 40 V level to the normal output levels.

A few seconds after turn-on, A5V1 conducts and shunts base current formerly available to A6Q7. A6Q7 collector current then decreases, allowing current to flow through the base of A6Q6. Series regulator A6Q10 then conducts only through the load impedance because the current path through A6CR5 and A6R6 is closed by limited A6Q7 base current.

The output voltage begins to rise as A6Q10 collector current flows into the load and charges C8B. When the output reaches +275 V , A5V1 shunts just enough current away from the base of A6Q7 to control the output current, maintaining a constant voltage regardless of the load impedance. The initial conditions hold until A5V1 begins to conduct appreciable current and the power supply outputs increase in voltage toward a stable condition.

When the -300 V supply output voltage increases more negative than -82 V , A5V2 turns on to regulate the A5Q1 and A5Q2A base voltages at this level. When the output voltage is -300 V , voltage at the center tap of A5R7-300V ADJ is set to -82 V and A5Q2A will take over control of the A6Q9 base current. This control establishes the stabilized -300 V output voltage.

Since the voltage difference between A5V1 cathode and A5CR14 cathode is less than 10V, A5CR17 prevents current from passing through A5R16 and into A5R22 when a stable condition is reached. This minimizes +275 V supply drift by reverse biasing A5CR15; i.e., there are no voltage variations across nonconducting A5CR15.

## +275V AND -300V POWER SUPPLY

## INTERDEPENDENCE.

When the +275 V supply output voltage exceeds +180 V , A5CR21 conducts, A5CR20 is reverse biased, and A5V1 is supplied with a well regulated plate voltage. A5V1 can conduct the proper current only if the -300 V supply voltage for A5R22, A5R23 and A5R26 is approximately correct. Thus, the +275 V supply is dependent on the -300 V supply for proper operation.

Further, the -300 V supply needs correct bias current supply by the +275 V supply. The -300 V supply sequences through the following states as the output voltage increases from -40 V to -300 V .

At turn-on, some of the A5R15 (next to test loop B) current flows through the base of A6Q9, turning on A6Q9, A6Q8 and the -300 V series regulator A6Q11. A6Q11 collector current passes through the -300V supply load impedance and develops an output voltage which is controlled by the relationship between A5R15, A5R16 and A5R22. Assuming that A6Q9 base current is negligible and that the voltage at A5CR14 cathode is always about 4.5 volts, the current flowing through A5R15 will also flow through A5R16 and A5R22 (A5V1 is off because filaments have not yet heated) and will develop a voltage at test point 1 about equal but of opposite polarity to the voltage at test point 2 , because the resistive sum of A5R22 and A5R16 is about equal to A5R15. The two power supply outputs approximately track each other during turn-on because equal currents flowing through equal resistances yield equal voltages. The small base current required by A6Q6 to maintain tracking is controlled by the voltage at either end of the A5R15/A5R16/A5R22 resistor stick.

## +275 AND -300V CURRENT LIMITERS.

The two current limiters are identical in function; the following paragraphs describe the +275 V current limiter. The current limiters are similar to a bridge circuit. A5Q4 acts as a switch to shunt base current away from A6Q6 which drives the series regulator, thus turning off the current available to the load. The unique characteristic of the circuit is that the maximum current available to the load is roughly proportional to output voltage.

Under normal operating conditions A5Q4 is turned off and the series regulator can have as much base current as it needs. If the load resistance begins to decrease so that the load current increases, A6Q10 emitter voltage increases due to the increase of voltage across A5R34. A5Q4 base voltage also increases and eventually exceeds A5Q4 emitter voltage. This turns on A5Q4, unbalances the bridge and provides a current path from the base of A6Q6 to the emitter of A5Q4, limiting the base current available to A6Q6.

Once A5Q4 collector current starts to flow, the output voltage decreases as series regulator A6Q10 base current is limited. A6Q7 will cut off as the feedback circuit tries to restore the output voltage, but the resulting extra base current available for the base of A6Q6 will be limited by the amount of A5Q4 collector current. With this limiting, the output voltage is no longer controlled by the feedback circuit, but is instead controlled by the current limiting circuit.

## +275V AND -300V VOLTAGE LIMITERS.

The two voltage limiters are identical in function; the following paragraphs describe the +275 V voltage limiter. The +275 V voltage limiting circuit works in conjunction with the +275 V current limiter to control voltage and current levels during all phases of turn-on, normal operation, and short circuit operation.

Under normal operating conditions, A5Q4 emitter ( +275 V output) is at +275 V so that the voltage difference between this point and the collectors of A6Q1 and A6Q3 is about 125V. (Maximum voltage at A6Q3 is +400 V at high line.) With only 125 V available, A6CR1 and A6CR2 will not conduct so that A6Q1 and A6Q3 will saturate. In this state, the voltage drop between the A6Q1/A6Q3 collectors and the collector of A6Q10 is nearly zero. Thus, the A6Q10 series regulator collector to emitter voltage is a maximum of 125 V ; a safe level for collector currents in excess of 200 mA .

If the +275 V supply load resistance should suddenly decrease to zero, A6Q10 emitter voltage will be about zero. A maximum of +400 V at A6F1 will drop across A6R1/A6R2/A6CR1/A6R15/A6CR2. A6CR1 and A6CR2 together drop approximately +140 V , leaving 260 V drop across A6R1 and A6R2. Disregarding A6Q1 base current, A6Q10 collector voltage level is then about 270 V , i.e., the collector voltage of A6Q10 is about the same as the voltage at the junction of A6R1 and A6R2. In this state, series regulator A6Q10 collector to emitter voltage will be about 270V. This is a safe level because the current limiter limits the current through A6Q10. A6CR1/A6CR2 and A6R1/A6R2 values are such that for any combination of load current and output voltage, the voltage across A6Q3 collector to emitter will be large enough to limit the series regulator power dissipation within safe limits.


3. Unplug A5 Assy. and Measure Resistance to Gnd. from XA5, PIN 12

4. Check Resistance Between PINS 12 and 14 on A5 Assy.

5. Check C8B and/or A5C11 and A5CR22


Figure 5-16. +275 V and -300V Power Supply Troubleshooting Flow (Continued)


Figure 5-16. +275V and -300V Power Supply Troubleshooting Flow (Continued)

1. Remove RF Unit, and All Plug-In P. C. Boards Except A5, A6, and A14

2. Check A6Q5-11
3. Move Test Loop B from Test Point \#2 to Test Point \#3

4. Trouble is in +275 V Supply. Check Diodes and Transistors with Ohmmeter. Check Current Limiter
5. Check Other Components with Ohmmeter
6. Return Test Loop B to Test Point 2
-300 V Supply
Voltage Incorrect

7. Return Test Loop B to Test Point 2
8. Check D. C. Voltages at A5V2 Cathode and A5CR4 Anode. Check Current Limiter

9. Check Resistors and Capacitors Associated with Above Components

Figure 5-16. +275 V and -300 V Power Supply Troubleshooting Flow (Continued)


Figure 5-16. +275V and -300V Power Supply Troubleshooting Flow (Continued)

## 7

1. Move Test Loop B from Test Point \#2 to Test Point \#3

2. Trouble is in +275 V

3. Check Gain of A6Q5, 6, 7, 10 4, 6, 7, 10 20, 23,
4. Check A5V1, CR17, 18, 20, 23, Q4, Q7
5. Check Gain of A6Q8, 9, 11
6. Temporarily Disconnect A5CR10 I
7. Check A5V2; C5; CR8, 9, 11, 16; R11; Q2, 3
High Ripple and/or Poor Regulation

8. Return Test Loop B to Test Point 2

Table 6-1. Reference Designation Index (Cont.)


Table 6-1. Reference Designation Index (Cont.)

| $\begin{gathered} \text { Reference } \\ \text { Designation } \\ \hline \end{gathered}$ | (10) Part No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| 4503 | 1854-0003 | TRANSISTOR:NPN SILICON |  |
| A 504 | 1854-0003 | TRANSISTOR:NPN SILICON |  |
| A5R1 | 0812-0018 | R:FXD WW 100 OHM 3\% 5W |  |
| A5R2 | 0819-0027 | R:FXD HH 10K OHM 5\% 20W |  |
| A5R3 | 0764-0031 | R:FXD MET OX 47K OHM 5\% 2W |  |
| A5R4 | 0812-0018 | R:FXD WW 100 OHM 3\% 5W |  |
| ASR5 | 0757-0856 | R:FXD MET FLM 75.0K OHM 1\% 1/2W |  |
| A5R6 | 0757-0460 | R:FXD MET FLM 61.9K OHM 18 1/8W |  |
| A 587 | 2100-1760 | R: VAR WH 5K OHM 10\% LIN 1/2W |  |
| A5R8 | 0757-0130 | R:FXD MET FLM 162K OHM 1\% 1/2W |  |
| A5R9 | 0757-0280 | R:FXD MET FLM 1K OHM 1\% $1 / 8 \mathrm{H}$ |  |
| A5R10 | 0698-3175 | R:FXD MET FLM 147K OHM 1\% 1/2W |  |
| A5R11 | 0757-0458 | R:FXD MET FLM 51.1K OHM $181 / 8 \mathrm{~W}$ |  |
| A5R12 | 0757-0463 | R:FXD MET FLM 82.5 K OHM 1\% $1 / 8 \mathrm{H}$ |  |
| A5R13 | 0764-0031 | R:FXD MET OX 47 K OHM 5\% 2 W |  |
| 5R14 | 0764-0031 | R:FXD MET OX 47 K OHM 5\% 2W |  |
| A5R15 | 0757-0133 | R:FXD MET FLM 383K OHM 2\% 1/2W |  |
| A5R16 | 0757-0465 | R:FXD MET FLM 100K OHM 1\% $1 / 8 \mathrm{H}$ |  |
| A5R17 | 0757-0063 | R:FXD MET FLM 196K OHM 1\% 1/2W |  |
| A5R18 | 0698-3444 | R:FXD MET FLM 316 OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A5R19 | 0698-0085 | R:FXD MET FLM 2.61K OHM 1\% 1/8W |  |
| A5R20 | 0757-0003 | R:FXD MET FLM 26.1 OHM $1 \% 1 / 2 \mathrm{~W}$ |  |
| A5R21 | 0757-0394 | R:FXD MET FLM 51.1 OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A5R22 | 0757-0064 | R:FXD MET FLM 261K OHM 1\% 1/2W |  |
| A5R23 | 0698-3425 | R:FXD MET FLM 316K OHM 1\% 1/2W |  |
| A5R24 | 0757-0465 | R:FXD MET FLM 100K OHM 1\% 1/8W |  |
| A5R25 | 0757-0442 | R:FXD MET FLM 10.0K OHM $1 \% 1 / 8 \mathrm{~W}$ |  |
| ASR26 | 0757-0129 | R:FXD MET FLM 178K OHM 2\% 1/2W |  |
| A5R27 | 2100-1760 | R: VAR WH 5K OHM 10\% LIN 1/2W | . |
| A5R28 | 0757-0279 | R:FXD MET FLM 3.16K OHM 1\% 1/8W |  |
| A5R29 | 0757-0367 | R:FXD MET FLM 100 K OHM 1\% $1 / 2 \mathrm{~W}$ |  |
| A5R30 | 0757-0280 | R:FXD MET FLM 1 K OHM $181 / 8 \mathrm{~W}$ |  |
| A5R31 | 0698-3437 | R:FXD MET FLM 133 OHM $181 / 8 \mathrm{~W}$ |  |
| A5R32 | 0698-3175 | R:FXD MET FLM 147K OHM 1\% 1/2W |  |
| - 5833 | 0757-0280 | R: FXD MET FLM 1 K OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A5834 | 0757-0984 | R:FXD MET FLM 10.0 OHM 18 1/2W |  |
| A5R35 | 0757-0130 | R:FXD MET FLM 162K OHM 1\% $1 / 2 \mathrm{~W}$ |  |
| A5R36 | 0698-3388 | R:FXD MET FLM 14.7 OHM 1\% 1/2W |  |
| 45837 | 0757-0394 | R:FXD MET FLM 51.1 OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A 5 VI | 1932-0030 | ELECTRON TUBE: 12AX7 |  |
| A5V2 | 1940-0013 | ELECTRON TUBE:82.0 +/- IV |  |
| A6 | 08690-6032 | BOARD ASSY:REGULATOR |  |
| $\mathrm{ABCl}^{1}$ | 0150-0052 | C:FXD CER 0.05 UF 208 400VDCW |  |

Table 6-1. Reference Designation Index (Cont.)

| $\begin{gathered} \text { Reference } \\ \text { Designation } \\ \hline \end{gathered}$ | (10) Part No. | Description \# | Note |
| :---: | :---: | :---: | :---: |
| A6C2 | 0150-0052 | C:FXD CER 0.05 UF 20\% 400VDCW |  |
| A6CR1 | 1902-3381 | DIODE BREAKDOWN:68.1V 400MW |  |
| AGCR2 | 1902-3381 | DIDDE BREAKDOWN:68.1V 400MW |  |
| A6CR 3 | 1901-0029 | DIODE:SILICON 600 PIV |  |
| A6CR 4 | 1902-0554 | DIODE BREAKDOWN:IOV 1W |  |
| A6CR 5 | 1901-0033 | DIODE:SILICON 100MA 180WV |  |
| A6CR6 | 1901-0033 | DIODE:SILICON 100MA 180WV |  |
| A6CR 7 | 1902-3381 | DIODE SREAKDOWN:68.1V 400MW |  |
| A6CR8 | 1902-3381 | DI ODE BREAKDOWN:68.1V 400MW |  |
| A6FI | 2110-0004 | FUSE:CARTRIDGE 1/4 AMP 250V |  |
| A6F2 | 2110-0004 | FUSE:CARTRIDGE 1/4 AMP 250V |  |
| A6Q1 | 1854-0232 | TRANSISTOR:SILICON NPN |  |
| A6Q2 | 1854-0232 | TRANSISTOR: SILICON NPN |  |
| A6Q3 | 1854-0237 | TRANSISTOR:SILICON NPN 2N3738 |  |
| A6Q4 | 1854-0237 | TRANSISTOR:SILICON NPN 2 N3738 |  |
| A6Q5 | 1854-0079 | TRANSISTOR:SILICON 2 N3439 |  |
| A6Q6 | 1854-0039 | TRANSISTOR:SILICON 2N3053 |  |
| A6Q7 | 1854-0079 | TRANSISTOR:SILICON 2N3439 |  |
| A6Q8 | 1854-0079 | TRANSISTOR:SILICON 2N3439 |  |
| A609 | 1854-0039 | TRANSISTOR:SILICON 2N3053 |  |
| A6010 | 1854-0080 | TRANSISTOR:SILICON |  |
| A6011 | 1854-0080 | TRANSISTOR:SILICON |  |
| A6R1 | 0757-0856 | R:FXD MET FLM 75.0K OHM 1\% 1/2W |  |
| A6R2 | 0757-0856 | R:FXD MET FLM 75.0K OHM 1\% 1/2W |  |
| A6R3 | 0757-0401 | R:FXD MET FLM 100 OHM 181/8W |  |
| A6R4 | 0757-0461 | R:FXD MET FLM 68.1 K OHM $181 / 8 \mathrm{~W}$ |  |
| A6R5 | 0757-0280 | R:FXD MET FLM 1 K OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A6R6 | 0811-0005 | R:FXD WW 1500 OHM 1\% 5W |  |
| A6R7 | 0757-0856 | R:FXD MET FLM 75.0K OHM 1\% 1/2W |  |
| A6R8 | 0757-0856 | R:FXD MET FLM 75.OK OHM 1\% 1/2W |  |
| A6R9 | 0757-0401 | R:FXD MET FLM 100 OHM $1 \% 1 / 8 \mathrm{~W}$ |  |
| A6R10 | 0757-0280 | R:FXD MET FLM $1 K$ OHM 1 / $1 / 8 \mathrm{~W}$ |  |
| A6R11 | 0757-0401 | R:FXD MET FLM 100 OHM 1\% $1 / 8 \mathrm{~W}$ |  |
| A6R12 | 0757-0401 | R:FXD MET FLM 100 OHM 1\% 1/8W |  |
| A6R13 A6R14 | 0757-0280 | R:FXD MET FLM $1 K$ DHM $1 \% 1 / 8 \mathrm{~W}$ R:FXD MET FLM $1 K$ OHM $1 \% 1 / 8 \mathrm{~W}$ |  |
| A6R14 | 0757-0280 | R:FXD MET FLM $1 K$ OHM $1 \% 1 / 8 \mathrm{~W}$ R:FXD MET FLM 3.16K OHM $1 \% 1 / 8 \mathrm{~W}$ |  |
| $\begin{aligned} & \text { AGR15 } \\ & \text { AGR16 } \end{aligned}$ | $\begin{aligned} & 0757-0279 \\ & 0757-0279 \end{aligned}$ | R:FXD MET FLM 3.16K OHM 1\% 1/8W R:FXD MET FLM 3.16K OHM 1\% $1 / 8 \mathrm{~W}$ |  |



